Mechanism reduction methods based on time scale separation

2nd part

Dimitris A. Goussis

National Technical University of Athens, Greece



Outline

- 1. Mathematical background
- 2. Time scales
- 3. Traditional reduction tools and their limitations
- 4. New algorithmic tools
- 5. Various methodologies
- 6. Applications
- 7. Quasi steady-state and partial equilibrium approx.



Some common features

 $\epsilon = 10^{-6}$





Obstacles for a successful asymptotic analysis

Given a system in dimensional form:

$$\frac{d\mathbf{y}}{dt} = \mathbf{g}(\mathbf{y};\mathbf{k})$$

When using the traditional tools a researcher must:

- 1. find all applicable *non-dimensional forms* of the system
- 2. transform all systems in *normal form*
- 3. determine the *sub-domain in phase space* where each system is valid
- 4. proceed with the *proper expansion* of variables
- 5. find a way to *match* the solution of the various systems



Theory of Singular Perturbations

Poincare, Stieltjes (1886, celestial mechanics)

Prandtl (1904, fluid mechanics)

Van der Pol (1920, circuits)

Tikhonov (1948), Levinson (1949)

Bogolubov, Carrier, Cole, van Dyke, Dorodnitsyn, Eckhaus, Hirsch, Holmes,

Fenichel, Friedrichs, Jones, Kaplun, Keller, Kevorkian, Lagerstrom, Mitropolsky,

O'Malley, Vasil'eva, Vehulst (from the 50's)



Geometrical Singular Perturbations

Hirsch, Fenichel, Pugh, Shub, Jones

Goals:

- Identify central dynamical *structures* in phase space
- Exploit their *properties*, such as fast slow decompositions

Basic tools:

- The *tangent space (the tangent bundle)*
- Fast and slow *sub-domains* of tangent space

(Tasso Kaper, AMS 1999)



The tangent space; its fast slow sub-domains

Lindemann, k_{1f}=10³, k_{1b}=10³, k₂=1





The tangent space; its fast slow sub-domains

Lindemann, k_{1f} =10³, k_{1b} =10³, k_2 =1





The tangent space; its fast slow sub-domains

Lindemann, k_{1f} =10³, k_{1b} =10³, k_2 =1





Lindemann mechanism: the fast and slow basis vectors

$$A + A \underset{k_{1b}}{\overset{k_{1f}}{\Leftrightarrow}} B + A \qquad B \underset{k_{1b}}{\overset{k_2}{\Rightarrow}} P$$

$$\frac{\mathrm{d}}{\mathrm{dt}}\begin{bmatrix} [\mathbf{B}]\\\\\\ [\mathbf{A}]\end{bmatrix} = \begin{bmatrix} +1\\\\\\-1\end{bmatrix} k_{1\mathrm{f}} [\mathbf{A}]^2 + \begin{bmatrix} -1\\\\\\+1\end{bmatrix} k_{1\mathrm{b}} [\mathbf{B}] [\mathbf{A}] + \begin{bmatrix} -1\\\\\\0\end{bmatrix} k_2 [\mathbf{B}]$$

$$\mathbf{a}_{1} = \begin{bmatrix} 1 \\ -\delta_{1} \end{bmatrix} \qquad \mathbf{a}_{2} = \begin{bmatrix} -\delta_{1}\delta_{2} \\ -1 \end{bmatrix} \qquad \delta_{1} = \left(1 + \frac{\mathbf{k}_{2}}{\mathbf{k}_{1b}[\mathbf{A}]}\right) \\ \delta_{2} = 2\frac{\mathbf{k}_{1f}}{\mathbf{k}_{1b}} - \frac{[\mathbf{B}]}{[\mathbf{A}]}$$



Lindemann mechanism: the reduced model

$$A + A \underset{k_{1b}}{\overset{k_{1f}}{\Leftrightarrow}} B + A \qquad B \xrightarrow{k_2} P$$

$$\frac{\mathrm{d}}{\mathrm{dt}}\begin{bmatrix} [B]\\ \\ [A]\end{bmatrix} = \begin{bmatrix} +1\\ \\ -1\end{bmatrix} k_{1\mathrm{f}}[A]^2 + \begin{bmatrix} -1\\ \\ +1\end{bmatrix} k_{1\mathrm{b}}[B][A] + \begin{bmatrix} -1\\ \\ 0\end{bmatrix} k_2[B]$$

$$(1+\delta_1\delta_2)^{-1}(k_{1f}[A]^2 - k_{1b}[B][A]) - k_2[B] \approx 0$$

$$\frac{d}{dt} \begin{bmatrix} [B] \\ [A] \end{bmatrix} \approx \begin{bmatrix} -\delta_1\delta_2 \\ -1 \end{bmatrix} \frac{\delta_1}{1+\delta_1^2\delta_2} \frac{k_{1f}}{k_{1b}} k_2[B]$$

$$\begin{split} \delta_1 = & \left(1 + \frac{k_2}{k_{1b}[A]}\right)^- \\ \delta_2 = & 2\frac{k_{1f}}{k_{1b}} - \frac{[B]}{[A]} \end{split}$$



Traditional vs new asymptotics

$$k_{1f}=10^3$$
 $k_{1b}=10^3$ $k_2=1$





Traditional vs new asymptotics

 $k_{1f}=10^3$ $k_{1b}=10^3$ $k_2=1$





Removing obstacles for a successful asymptotic analysis

Given a system in dimensional form:

$$\frac{d\mathbf{y}}{dt} = \mathbf{g}(\mathbf{y};\mathbf{k})$$

When using the new algorithms a researcher does not have to:

- 1. find all applicable non-dimensional forms of the system
- 2. transform all systems in *normal form*
- 3. determine the *sub-domain in phase space* where each system is valid
- 4. proceed with the proper expansion of variables
- 5. find a way to *match* the solution of the various systems

Instead, he has to:

- 1. find the fast and slow basis vectors of the tangent space
- 2. find ways to *efficiently* use them



Model reduction

$$\frac{d\mathbf{y}}{dt} = \mathbf{g}(\mathbf{y})$$

$$\frac{d\mathbf{y}}{dt} = \begin{bmatrix} \mathbf{a}_1 & \dots & \mathbf{a}_M \end{bmatrix} \begin{pmatrix} \mathbf{b}^1 \\ \vdots \\ \mathbf{b}^M \end{bmatrix} \mathbf{g}(\mathbf{y}) + \begin{bmatrix} \mathbf{a}_{M+1} & \dots & \mathbf{a}_N \end{bmatrix} \begin{pmatrix} \mathbf{b}^{M+1} \\ \vdots \\ \mathbf{b}^N \end{bmatrix} \mathbf{g}(\mathbf{y}) = \mathbf{a}_r \mathbf{f}^r + \mathbf{a}_s \mathbf{f}^s$$

$$\mathbf{a}_r \mathbf{f}^r = \mathbf{b}^r \mathbf{g}(\mathbf{y})$$

$$\mathbf{f}^r = \mathbf{b}^r \mathbf{g}(\mathbf{y})$$

$$\mathbf{f}^s = \mathbf{b}^s \mathbf{g}(\mathbf{y})$$



Problems

- 1. Complex structures
- 2. Variation of M with time/space
- 3. Evaluation of **a**_i
- 4. Solving the algebraic eqs.



τ

Model reduction

$$\frac{d\mathbf{y}}{dt} = \mathbf{g}(\mathbf{y})$$

$$\frac{d\mathbf{y}}{dt} = \begin{bmatrix} \mathbf{a}_1 & \dots & \mathbf{a}_M \end{bmatrix} \begin{pmatrix} \mathbf{b}^1 \\ \vdots \\ \mathbf{b}^M \end{bmatrix} \mathbf{g}(\mathbf{y}) + \begin{bmatrix} \mathbf{a}_{M+1} & \dots & \mathbf{a}_N \end{bmatrix} \begin{pmatrix} \mathbf{b}^{M+1} \\ \vdots \\ \mathbf{b}^N \end{bmatrix} \mathbf{g}(\mathbf{y}) = \mathbf{a}_r \mathbf{f}^r + \mathbf{a}_s \mathbf{f}^s$$

$$\mathbf{a}_r \mathbf{f}^r = \mathbf{b}^r \mathbf{g}(\mathbf{y})$$

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Problems

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τ

Structures in tangent space





Structures in tangent space

u = 0 -2 -4 -2 0 -2 -4 -2 -4 -2 -4 -2 -4 -2 -4 -2 -4 -2 -4 -2 -4 -2 -4 -2 -4 -2 -4 -2 -4

van der Pol

$$\frac{du}{dt} = -x$$
$$\frac{dx}{dt} = \frac{1}{\varepsilon} \left(u - x - \frac{x^3}{3} \right)$$



$$\frac{dx}{dt} = -y - z$$
$$\frac{dy}{dt} = x + ay$$
$$\frac{dz}{dt} = b + z(x - c)$$



Structures in tangent space





Bykov & Maas, CTM 2007



Model reduction

$$\frac{d\mathbf{y}}{dt} = \mathbf{g}(\mathbf{y})$$

$$\frac{d\mathbf{y}}{dt} = \begin{bmatrix} \mathbf{a}_1 & \dots & \mathbf{a}_M \end{bmatrix} \begin{pmatrix} \mathbf{b}^1 \\ \vdots \\ \mathbf{b}^M \end{bmatrix} \mathbf{g}(\mathbf{y}) + \begin{bmatrix} \mathbf{a}_{M+1} & \dots & \mathbf{a}_N \end{bmatrix} \begin{pmatrix} \mathbf{b}^{M+1} \\ \vdots \\ \mathbf{b}^N \end{bmatrix} \mathbf{g}(\mathbf{y}) = \mathbf{a}_r \mathbf{f}^r + \mathbf{a}_s \mathbf{f}^s$$

$$\mathbf{f}^r = \mathbf{b}^r \mathbf{g}(\mathbf{y})$$

$$\mathbf{f}^s = \mathbf{b}^s \mathbf{g}(\mathbf{y})$$



Problems

- 1. Complex structures
- 2. Variation of M with time/space
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Number of fast time scales H_2/air





Number of fast time scales DME/air (1100K)





Number of fast time scales DME/air (900K)





Number of fast time scales n-hexane/air (600K)





Number of fast time scales CH_4/air



Temperature

Valorani et al, C&F 2003



Number of fast time scales CH₄/air





Number of fast time scales CH₄/air





Model reduction

$$\frac{d\mathbf{y}}{dt} = \mathbf{g}(\mathbf{y})$$

$$\frac{d\mathbf{y}}{dt} = \begin{bmatrix} \mathbf{a}_1 & \dots & \mathbf{a}_M \end{bmatrix} \begin{pmatrix} \mathbf{b}^1 \\ \vdots \\ \mathbf{b}^M \end{bmatrix} \mathbf{g}(\mathbf{y}) + \begin{bmatrix} \mathbf{a}_{M+1} & \dots & \mathbf{a}_N \end{bmatrix} \begin{pmatrix} \mathbf{b}^{M+1} \\ \vdots \\ \mathbf{b}^N \end{bmatrix} \mathbf{g}(\mathbf{y}) = \mathbf{a}_r \mathbf{f}^r + \mathbf{a}_s \mathbf{f}^s$$

$$\mathbf{f}^r = \mathbf{b}^r \mathbf{g}(\mathbf{y})$$

$$\mathbf{f}^s = \mathbf{b}^s \mathbf{g}(\mathbf{y})$$



Problems

- 1. Complex structures
- 2. Variation of M with time/space
- 3. Evaluation of **a**_i
- 4. Solving the algebraic eqs.



Finding the fast and slow basis vectors

 Fenichel, Indiana Univ. Math. J.,
 23:1109-1137 (1971)

 J. Differential Equations,
 31:53-98 (1979)

Lam and Goussis CSP (1988) Maas and Pope ILDM (1992) Valorani et al. NTDB (2006)

Roussel and Fraser (1988)[Goussis and Valorani (2006)]Gear and Kevrekidis (2005)[Zagaris, Kaper and Kaper (2005)]Gorban and Karlin (2003)Contou and Daoutidis (2008)



Computing the fast and slow basis vectors





Computing the fast and slow basis vectors





Model reduction

$$\frac{d\mathbf{y}}{dt} = \mathbf{g}(\mathbf{y})$$

$$\frac{d\mathbf{y}}{dt} = \begin{bmatrix} \mathbf{a}_1 & \dots & \mathbf{a}_M \end{bmatrix} \begin{pmatrix} \mathbf{b}^1 \\ \vdots \\ \mathbf{b}^M \end{bmatrix} \mathbf{g}(\mathbf{y}) + \begin{bmatrix} \mathbf{a}_{M+1} & \dots & \mathbf{a}_N \end{bmatrix} \begin{pmatrix} \mathbf{b}^{M+1} \\ \vdots \\ \mathbf{b}^N \end{bmatrix} \mathbf{g}(\mathbf{y}) = \mathbf{a}_r \mathbf{f}^r + \mathbf{a}_s \mathbf{f}^s$$

$$\mathbf{f}^r = \mathbf{b}^r \mathbf{g}(\mathbf{y})$$

$$\mathbf{f}^s = \mathbf{b}^s \mathbf{g}(\mathbf{y})$$



Problems

- 1. Complex structures
- 2. Variation of M with time/space
- 3. Evaluation of **a**_i
- 4. Solving the algebraic eqs.



n-heptane





Premixed flames: skeletal vs reduced





Premixed flames: skeletal vs reduced





Run time





Model reduction

$$\frac{d\mathbf{y}}{dt} = \mathbf{g}(\mathbf{y})$$

$$\frac{d\mathbf{y}}{dt} = \begin{bmatrix} \mathbf{a}_1 & \dots & \mathbf{a}_M \end{bmatrix} \begin{pmatrix} \mathbf{b}^1 \\ \vdots \\ \mathbf{b}^M \end{bmatrix} \mathbf{g}(\mathbf{y}) + \begin{bmatrix} \mathbf{a}_{M+1} & \dots & \mathbf{a}_N \end{bmatrix} \begin{pmatrix} \mathbf{b}^{M+1} \\ \vdots \\ \mathbf{b}^N \end{bmatrix} \mathbf{g}(\mathbf{y}) = \mathbf{a}_r \mathbf{f}^r + \mathbf{a}_s \mathbf{f}^s$$

$$\mathbf{f}^r = \mathbf{b}^r \mathbf{g}(\mathbf{y})$$

$$\mathbf{f}^s = \mathbf{b}^s \mathbf{g}(\mathbf{y})$$



Problems

- 1. Complex structures
- 2. Variation of M with time/space
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- 4. Solving the algebraic eqs.



Diagnostics

$$\begin{aligned} \frac{d\mathbf{y}}{dt} &= \mathbf{S}_{1}\mathbf{R}^{1} + \mathbf{S}_{2}\mathbf{R}^{2} + \ldots + \mathbf{S}_{K}\mathbf{R}^{K} = \mathbf{g}(\mathbf{y}) \\ \frac{d\mathbf{y}}{dt} &= \mathbf{a}_{r}\mathbf{f}^{r} + \mathbf{a}_{s}\mathbf{f}^{s} = \left(\mathbf{a}_{1}\mathbf{f}^{1} + \ldots + \mathbf{a}_{M}\mathbf{f}^{M}\right) + \left(\mathbf{a}_{M+1}\mathbf{f}^{M+1} + \ldots + \mathbf{a}_{N}\mathbf{f}^{N}\right) \qquad \mathbf{f}^{i} = \mathbf{b}^{i} \cdot \mathbf{g} \\ &= 0 \end{aligned}$$

$$\mathbf{f}^{i} &= \left(\mathbf{b}^{i} \cdot \mathbf{S}_{1}\right)\mathbf{R}^{1} + \left(\mathbf{b}^{i} \cdot \mathbf{S}_{2}\right)\mathbf{R}^{2} + \ldots + \left(\mathbf{b}^{i} \cdot \mathbf{S}_{K}\right)\mathbf{R}^{K} = 0 \qquad i = 1, M \end{aligned}$$

$$\mathbf{f}^{i} &= \left(\mathbf{b}^{i} \cdot \mathbf{S}_{1}\right)\mathbf{R}^{1} + \left(\mathbf{b}^{i} \cdot \mathbf{S}_{2}\right)\mathbf{R}^{2} + \ldots + \left(\mathbf{b}^{i} \cdot \mathbf{S}_{K}\right)\mathbf{R}^{K} \neq 0 \qquad i = M+1, N \end{aligned}$$

$$\mathbf{\tau}_{i} &= \left(\mathbf{b}^{i} \cdot \mathbf{S}_{1}\right)\left(\nabla \mathbf{R}^{1} \cdot \mathbf{a}_{i}\right) + \ldots + \left(\mathbf{b}^{i} \cdot \mathbf{S}_{K}\right)\left(\nabla \mathbf{R}^{K} \cdot \mathbf{a}_{i}\right) \qquad i = 1, N \end{aligned}$$





Diamantis et al, CTM 2015







2 0	·	·		$t = 2.000 \times 10^{-5} \text{ s}$ T = 1100 K $\lambda = 3.251 \times 10^{5} \text{ s}^{-1}$	$t = 4.500 \times 10^{-5} \text{ s}$ T = 1168 K $\lambda = 7.014 \times 10^{5} \text{ s}^{-1}$	$t = 4.782 \times 10^{-5} \text{ s}$ T = 1593 K $\lambda = 3.043 \times 10^{5} \text{ s}^{-1}$	
3e-0 τ _i 2e-0	06 - 06 - Li model		- TPI	$\begin{array}{r} 1f: + \ 0.6265\\ 2f: + \ 0.0740\\ 3f: + \ 0.0184\\ 9f: - \ 0.2785\end{array}$	$\begin{array}{r} 1f: + \ 0.5959\\ 2f: + \ 0.1430\\ 3f: + \ 0.0886\\ 11f: + \ 0.0543\\ 10f: - \ 0.0316\\ 1b: - \ 0.0304\\ 8f: - \ 0.0210 \end{array}$	$\begin{array}{r} 1f: + \ 0.2652\\ 2f: + \ 0.1607\\ 3f: + \ 0.0569\\ 8f: + \ 0.0277\\ 1b: - \ 0.1581\\ 2b: - \ 0.1244\\ 3b: - \ 0.0853 \end{array}$	
1e-0 0e+0			API	$\begin{array}{r} 1f: + \ 0.6265\\ 2f: + \ 0.0740\\ 3f: + \ 0.0184\\ 9f: - \ 0.2785 \end{array}$	$\begin{array}{r} 1f: + \ 0.5823\\ 2f: + \ 0.1408\\ 3f: + \ 0.0972\\ 11f: + \ 0.0723\\ 10f: - \ 0.0414\\ 1b: - \ 0.0173\\ 8f: - \ 0.0126 \end{array}$	$\begin{array}{r} 1f: + \ 0.3389\\ 2f: + \ 0.1646\\ 3f: + \ 0.1432\\ 9f: + \ 0.0704\\ 8f: + \ 0.0598\\ 1b: - \ 0.0838\\ 2b: - \ 0.0515\\ 3b: - \ 0.0366\\ \end{array}$	
	0 2e-0	5 4e-05 6e-0. time	5 Po	H: + 0.79 O: + 0.17	H: + 0.65 T: + 0.19	T: +3.50 $O_2: -2.60$ $H_2O: -2.45$	
					0:+0.13		
	$1f - EN$ $H + O_2 \rightarrow O + OH$			$1b - EX$ $H + O_2 \leftarrow O + OH$			
	$2f - EN$ $O + H_2 \rightarrow H + OH$			$2b - EX$ $O + H_2 \leftarrow H + OH$			
	$3f - EX$ $OH + H_2 \rightarrow H + H_2O$			$3b - EN$ $OH + H_2 \leftarrow H + H_2O$			
	$8f - EX$ $H + OH(+M) \rightarrow H_2O(+M)$			9f-E	$9f - EX$ $H + O_2(+M) \rightarrow HO_2(+M)$		r . ,
$10f - EX$ $H + HO_2 \rightarrow H_2 + O$			$_{2} + O_{2}$	10b - E	H + 1	$\mathrm{HO}_2 \leftarrow \mathrm{H}_2 + \mathrm{O}_2$	
$11f - EX$ $H + HO_2 \rightarrow OH + OH$			I + OH				





Chemical vs thermal runaway regime



Algorithms

- 1. Computational Singular Perturbation (CSP)
- 2. Intrinsic Low-Dimensional Manifolds (ILDM)
- 3. In Situ Adaptive Tabulation (ISAT)
- 4. Reaction Diffusion Manifolds (REDIM)

CSP: Proc. Combust. Inst., 22:931-941 (1988), Int. J. Chem. Kinet., 26:461-486 (1994)

- ISAT: Combust. Theory Model., 1:41-63 (1977), J. Comp. Phys., 228:361-386 (2009)
- ILDM: Proc. Combust. Inst., 24:103-112 (1992), Proc. Combust. Inst., 25:1349-1356 (1994)
- REDIM: Proc. Combust. Inst., 31:465-472 (2007), Proc. Combust. Inst., 34:197-203 (2013)



Computational Singular Perturbation (CSP) algorithm

$$\mathbf{a}_{r}^{o} = [\mathbf{a}_{1}^{o} \dots \mathbf{a}_{N}^{o}] \qquad \mathbf{a}_{s}^{o} = [\mathbf{a}_{M+1}^{o} \dots \mathbf{a}_{N}^{o}]$$
$$\mathbf{b}_{o}^{r} = \begin{bmatrix} \mathbf{b}_{o}^{1} \\ \vdots \\ \mathbf{b}_{o}^{M} \end{bmatrix} \qquad \mathbf{b}_{o}^{s} = \begin{bmatrix} \mathbf{b}_{o}^{M+1} \\ \vdots \\ \mathbf{b}_{o}^{N} \end{bmatrix}$$

$$\begin{bmatrix} \mathbf{b}_{o}^{r} \\ \mathbf{b}_{o}^{s} \end{bmatrix} \begin{bmatrix} \mathbf{a}_{r}^{o} & \mathbf{a}_{s}^{o} \end{bmatrix} = \begin{bmatrix} \mathbf{I}_{M}^{M} & \mathbf{0}_{N-M}^{M} \\ \mathbf{0}_{N}^{N-M} & \mathbf{I}_{N-M}^{N-M} \end{bmatrix}$$

$$\mathbf{a}_{r}$$
 - refinement:
 $\mathbf{a}_{r} = \left(\frac{d\mathbf{a}_{r}^{o}}{dt} + \mathbf{J}\mathbf{a}_{r}^{o}\right)\mathbf{k}_{r}^{r}$

b^r- refinement:

$$\mathbf{b}^{r} = \mathbf{k}_{r}^{r} \left(\frac{d\mathbf{b}_{o}^{r}}{dt} + \mathbf{b}_{o}^{r} \mathbf{J} \right)$$

$$\mathbf{k}_{\mathrm{r}}^{\mathrm{r}} = \left[\mathbf{b}_{o}^{r} \left(\frac{d\mathbf{a}_{r}^{o}}{dt} + \mathbf{J}\mathbf{a}_{r}^{o}\right)\right]^{-1}$$



H2/air and n-heptane/air ignition





Implicit Low Dimensional Manifolds (ILDM) algorithm

$$\mathbf{a}_{r}$$
 - refinement:
 $\mathbf{a}_{r} = \left(\frac{d\mathbf{a}_{r}^{o}}{dt} + \mathbf{J}\mathbf{a}_{r}^{o}\right)\mathbf{k}_{r}^{r}$

b^r- refinement:

$$\mathbf{b}^{r} = \mathbf{k}_{r}^{r} \left(\frac{d\mathbf{b}_{o}^{r}}{dt} + \mathbf{b}_{o}^{r} \mathbf{J} \right)$$

$$\mathbf{k}_{\mathrm{r}}^{\mathrm{r}} = \left[\mathbf{b}_{o}^{r} \left(\frac{d\mathbf{a}_{r}^{o}}{dt} + \mathbf{J}\mathbf{a}_{r}^{o}\right)\right]^{-1}$$

ignore d/dt

$$\mathbf{a}_r^O = \mathbf{\alpha}_r$$
 $\mathbf{b}_O^r = \mathbf{\beta}^r$

$$\mathbf{a}_{r} = \left(\mathbf{J}\mathbf{a}_{r}^{O}\right)\mathbf{k}_{r}^{r} = \left(\mathbf{J}\boldsymbol{\alpha}\right)\left[\boldsymbol{\beta}^{r}\mathbf{J}\boldsymbol{\alpha}\right]^{-1} = \left(\boldsymbol{\alpha}\boldsymbol{\lambda}\right)\left[\boldsymbol{\lambda}\right]^{-1} = \boldsymbol{\alpha}$$



Implicit Low Dimensional Manifolds (ILDM) algorithm

Tabulate $\boldsymbol{y}^{\text{M}},\,\boldsymbol{\alpha}_{\text{r}}$ and $\boldsymbol{\beta}^{\text{r}}$ in phase space of $\boldsymbol{y}^{\text{N-M}}$



FIG. 4. Calculated structure of a syngas-air flame (points: reduced mechanism, lines: detailed mechanism).

Maas and Pope, Proc. CI, 1994



Transport



Fig. 1. Schematical illustration of the time scales governing a chemically reacting flow.

Maas & Pope, C&F 1992



Transport

$$\frac{d\mathbf{y}}{dt} = \mathbf{S}_1 \mathbf{R}^1 + \mathbf{S}_2 \mathbf{R}^2 + \dots + \mathbf{S}_K \mathbf{R}^K + \mathbf{q} \nabla^2 \mathbf{y} = \mathbf{g}(\mathbf{y}) + \mathbf{q} \nabla^2 \mathbf{y}$$

$$\frac{d\mathbf{y}}{dt} = \mathbf{a}_r \mathbf{f}^r + \mathbf{a}_s \mathbf{f}^s = (\mathbf{a}_1 \mathbf{f}^1 + \dots + \mathbf{a}_M \mathbf{f}^M) + (\mathbf{a}_{M+1} \mathbf{f}^{M+1} + \dots + \mathbf{a}_N \mathbf{f}^N)$$

$$= 0 \qquad \qquad \mathbf{f}^i = \mathbf{b}^i \cdot (\mathbf{g} + \mathbf{q} \nabla^2 \mathbf{y})$$

Maas and Pope, Proc. CI, 1994 Hadjinicolaou and Goussis, SIAM MMS, 1998



In Situ Adaptive Calculation

Tabulate y^{M} , α_{r} and β^{r} in "useful" part of phase space of y^{N-M}



Linear approximation of known quantity or Computation from full model

> Pope, CTM, 1997 Tang and Pope, Proc. CI, 2002 Singer, Pope and Najm, CF, 2006 Lu and Pope, JCP, 2007



Conclusions

Model reduction is still an open field

- [1] A. Tomlin, T. Turányi, and M. Pilling, *Mathematical tools for the construction, investigation and reduction of combustion mechanisms*, in *Low Temperature Combustion and Autoignition*, M. Pilling and G. Hancock, eds., Elsevier, Amsterdam, 1997, pp. 293–437.
- [2] D.A. Goussis and U. Maas, *Model reduction for combustion chemistry*, in *Turbulent Combustion Modeling*, T. Echekki and E. Mastorakos, eds., Springer, New York, 2011, pp. 193–220.
- [3] T. Lovas, *Model reduction techniques for chemical mechanisms*, in *Chemical Kinetics*, V. Patel, ed., InTech, Croatia, 2012, pp. 79–114.
- [4] U. Maas and A.S. Tomlin, *Time-scale splitting-based mechanism reduction*, in *Cleaner Combustion Green Energy and Technology*, F. Battin-Leclerc, J.M. Simmie, and E. Blurock, eds., Springer, London, 2013, pp. 467–484.
- [5] T. Turányi and A.S. Tomlin, *Analysis of Kinetic Reaction Mechanisms*, Springer, Heidelberg, 2014.

